Design process for 12v -> 24v 200mA regulator using LM2577-ADJ

See National Semiconductor LM1577/LM2577 Simple Switcher specification sheet / application note DS011468 (June 1999) Starting from circuit on p12:

Vin(min) = 12; Vout = 24; Iload(max) = 0.2

Vout required is less than both limits of 60V & 10 * 12 = 120V

Limit for Iload(max) is (2.1 * 12) / 24 = 1.05A (well above 0.2A required)

Inductor selection

D(max) = (24 + 0.5 - 12) / (24 + 0.5 - 0.6) = 0.52

E * T = (0.52 * (12 - 0.6) * 1000000) / 52000 = 114.65

Iind,dc = (1.05 * 0.2) / (1 - 0.52) = 0.44

From fig 9, inductor code is H1000

As D is < 0.85, go to step C

Inductor H1000 (1000µH) is Schott 67127110, Pulse PE-53120 or Renco RL1959.

Avoid Renco as they generate more EMI.

Compensation network

 $Rc < (750 * 0.2 * 24 * 24) / (12 * 12) = 600\Omega$

Rc must lie between this value and 3k. Choose $1k\Omega$.

Cout > $(0.19 * 0.001 * 1000 * 0.2) / (12 * 24) = 132 \mu F$

and

 $Cout > (12 * 1000 * (12 + (3.74 * 100000 * 0.001))) / (487800 * 24 * 24 * 24) = 686 \mu F$

Choose 1000µF.

Working voltage must be at least 30V.

Iripple(rms) = (0.2 * 0.52) / (1 - 0.52) = 0.22A

Ripple current rating must be at least 0.35A at 52kHz.

Equivalent series resistance is minimised by choosing capacitors above 470μF, with high WVDC.

Dubilier 239, 250, 251, UFT, 300, 350

Nichicon PF, PX, PZ

Sprague 672D, 673D, 674D

United Chemi-Con LX, SXF, SXJ

 $Cc > (58.5 * 24 * 24 * 0.00075) / (1000000 * 12) = 2.1 \mu F$

Choose 3.3µF.

Vout = 1.23 * (1 + R1 / R2); transposing, R1 / R2 = (24 / 1.23) - 1 = 18.51

Close approximation to ratio yielded by preferred values $R1 = 56k\Omega$ & $R2 = 3k\Omega$ giving a nominal output of 24.19V. With 1% tolerance resistors, actual output voltage could be from 23.74V (R1 low, R2 high) to 24.65V (R1 high, R2 low).

Cin: 0.1µF good quality with short leads, plus 47µF electrolytic in parallel.

Diode: Schottky recommended; 30V 1A types 1N5818, MBR130P, 11DQ03

